



## Metrology infrastructure for high-pressure gas and liquified hydrogen flows

# **Alternative fluid calibration**

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- the idea is to use critical flow Venturi nozzles (CFVNs) as secondary standards (ISO 9300)
- identification of potential alternative gas in calibration of CFVNs used with hydrogen
- the ideal mass flow rate of the fluid through the nozzle is given by:

 $\boldsymbol{q}_{m,id} = \frac{\boldsymbol{A}\boldsymbol{C}^{*}\boldsymbol{\rho}_{0}}{\sqrt{\boldsymbol{R}_{m}\boldsymbol{T}_{0}}}$ 

the discharge coefficient

$$C_d = rac{q_m}{q_{m,id}} pprox a \left( 1 - rac{b}{\sqrt{Re}} 
ight)$$

ISO 9300 (toroidal nozzle):
 a = 0.9985, b = 3.412 and n = 0.5



#### **Test setup & test procedure**







# **Experimental results**





- similar trends of C<sub>d</sub> for different gases are observed for both nozzles
- $C_d$  for air, N<sub>2</sub> and H<sub>2</sub> almost overlap
- based on the experimental results the gases can be classified into three groups:
  - (i) He and Ar ( $\kappa$ =1.67) (ii) air, N<sub>2</sub> and H<sub>2</sub> ( $\kappa$ =1.4) (iii) N<sub>2</sub>O ( $\kappa$ =1.3)

# Analysis of the results



deviations relative to N<sub>2</sub>

 $\epsilon = C_d^{( ext{predicted})} \ / \ C_d^{( ext{actual})} - 1$ 



- prediction of  $C_d$  based on N<sub>2</sub> calibration
- using analytical models (e.g. Kligel-Levine & Gerop), which take into account κ and Pr





- $C_d$  for H<sub>2</sub> agrees well with  $C_d$  of air and N<sub>2</sub>
- $C_d$  was found to be dependent on isentropic coefficient ( $\kappa$ )
- difference can be explained using analytical models taking into account the actual properties of gases (except N<sub>2</sub>O)
- in the laminar boundary layer regime the CFVN can potentially be calibrated with alternative gases → first choice air and N<sub>2</sub>
- second option is to use other gas (e.g. helium) and then use the theoretical models to predict the behaviour (higher uncertainty)



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